

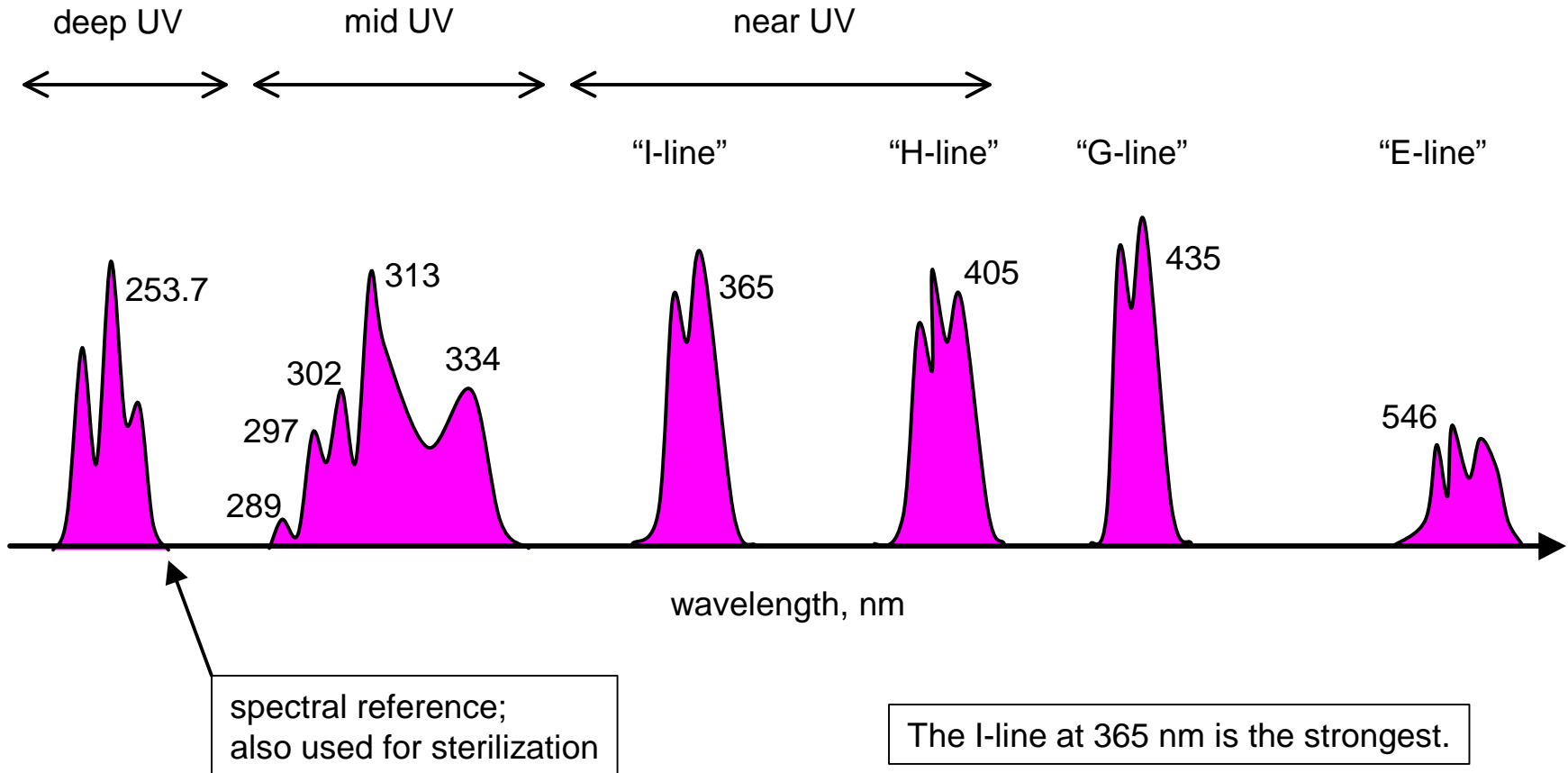
EE-527: MicroFabrication

Exposure and Imaging

Exposure Sources

- Photons
 - white light
 - Hg arc lamp
 - filtered Hg arc lamp
 - excimer laser
 - x-rays from synchrotron
- Electrons
 - focused electron beam direct write
- Ions
 - focused ion beam direct write

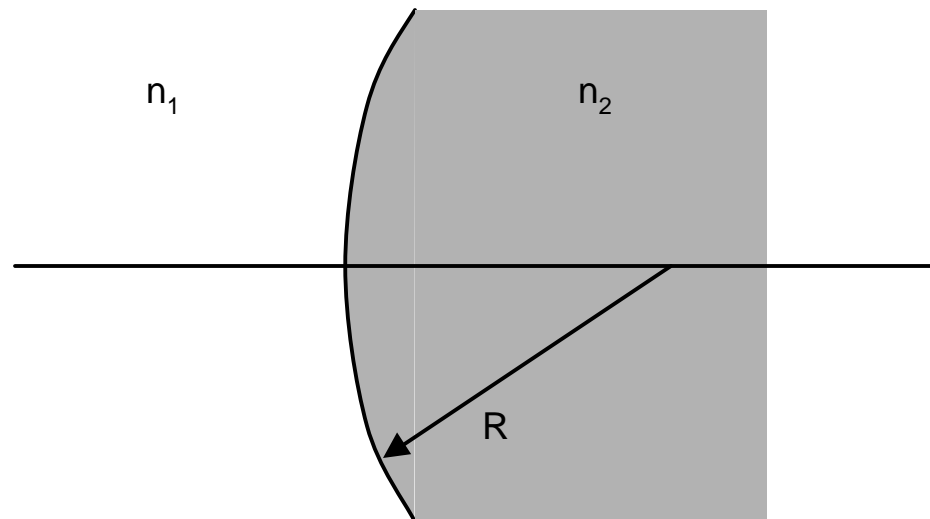
High Pressure Hg Arc Lamp Spectrum



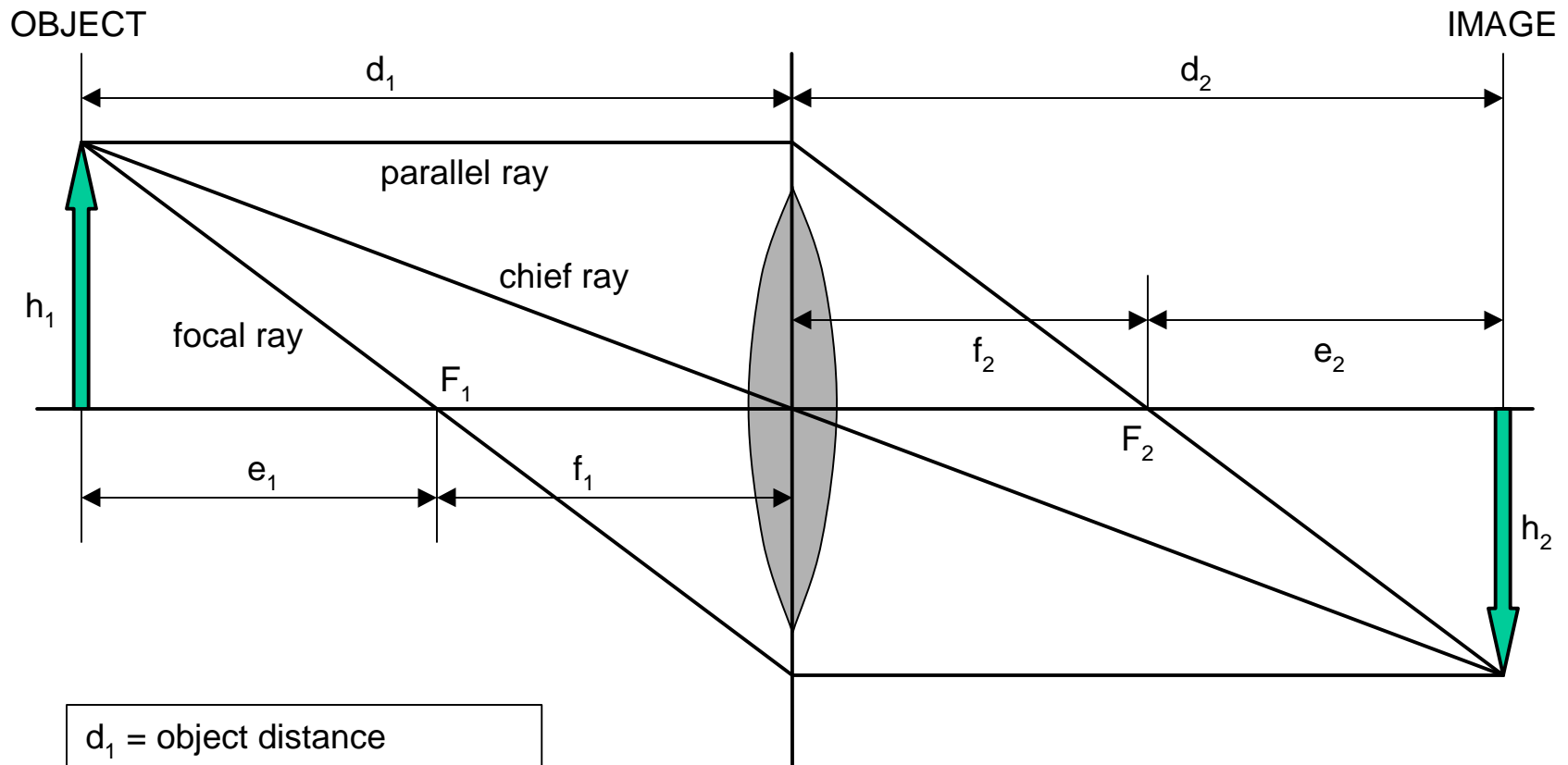
Refractive Power of a Surface

- The refractive power P is measured in diopters when the radius is expressed in meters.
- n_1 and n_2 are the refractive indices of the two media.

$$P = \frac{n_2 - n_1}{R}$$

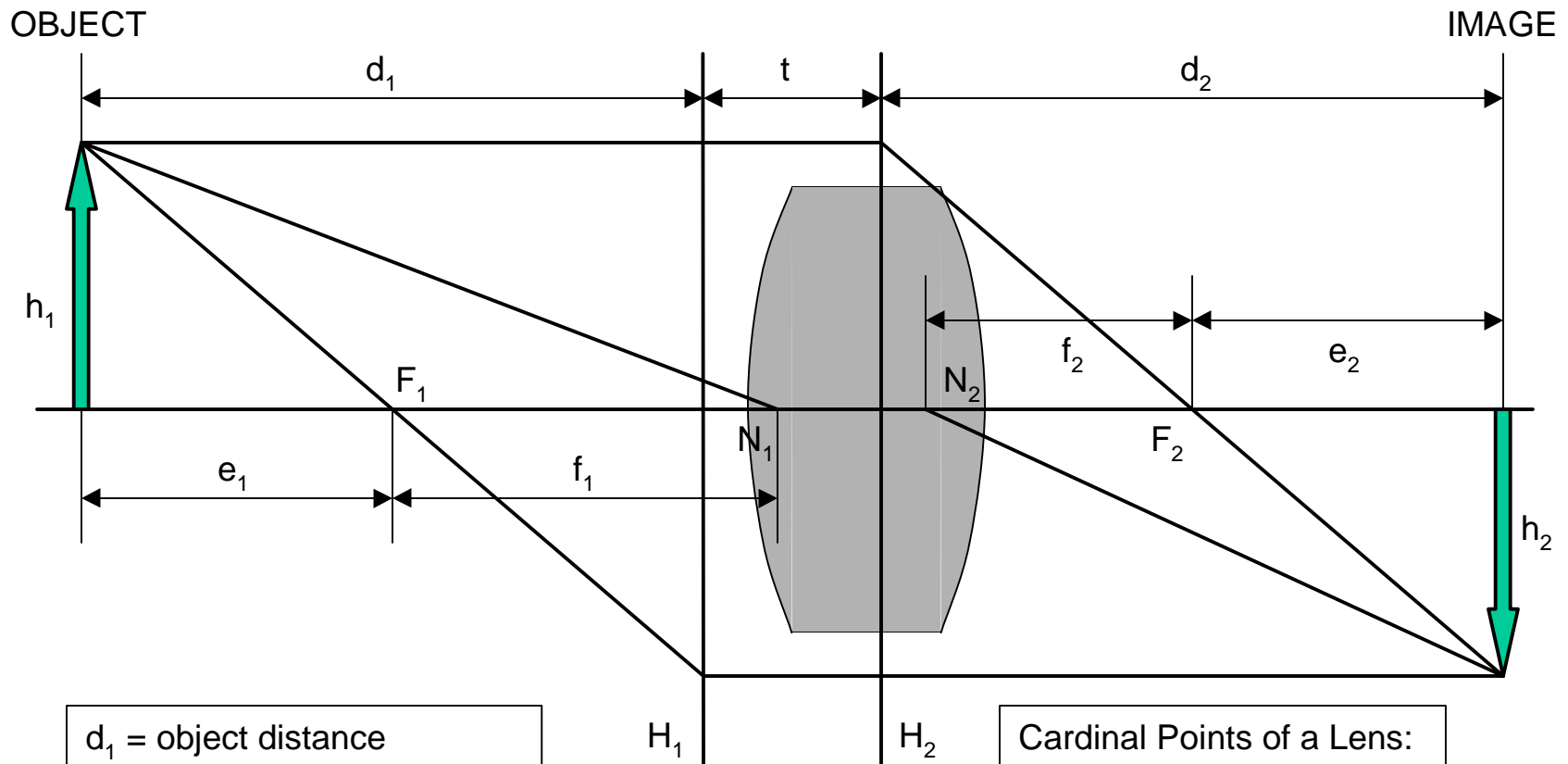


Thin Lenses



d_1 = object distance
 d_2 = image distance
 f_1, f_2 = focal lengths
 e_1, e_2 = extrafocal distances
 h_1, h_2 = object/image heights

Thick Lenses



d_1 = object distance
 d_2 = image distance
 f_1, f_2 = focal lengths
 e_1, e_2 = extrafocal distances
 h_1, h_2 = object/image heights

Cardinal Points of a Lens:
 Focal Points: F_1, F_2
 Nodal Points: N_1, N_2
 Principal Points: H_1, H_2

Lens-Maker's Formula

$$\frac{n_1}{d_1} + \frac{n_2}{d_2} = \frac{n - n_1}{R_1} + \frac{n - n_2}{R_2}$$

If $n_1 = n_2 = 1$, then

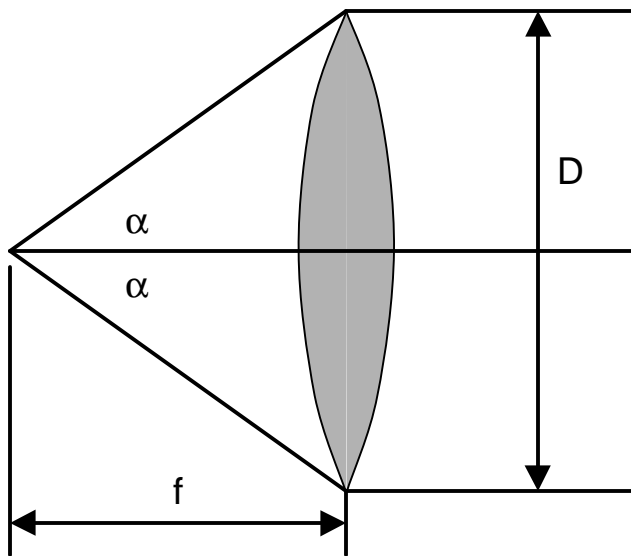
$$\frac{1}{d_1} + \frac{1}{d_2} = (n - 1) \left(\frac{1}{R_1} + \frac{1}{R_2} \right) = P = \frac{1}{f}$$

This can also be expressed as: $(d_1 - f)(d_2 - f) = f^2$

or: $e_1 e_2 = f^2$

Lens Apertures

- The f-number of a lens ($f/\#$) is the focal length divided by the diameter. It is a measure of the light gathering ability.
- The numerical aperture (NA) of a lens is $n \cdot \sin \alpha$, where α is the half-angle of the largest cone of light entering the lens.



$$f/\# = \frac{f}{D}$$

$$NA = n \sin \alpha$$

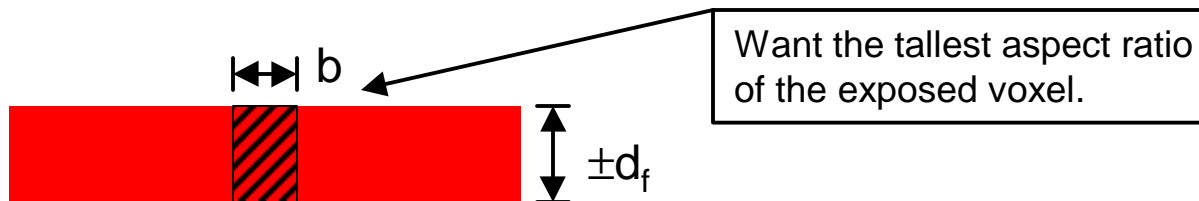
$$NA = \frac{\frac{1}{2}D}{\sqrt{\frac{1}{4}D^2 + f^2}} \approx \frac{D}{2f} = \frac{1}{2 \cdot f/\#}$$

Resolving Power of a Lens

- Rayleigh criterion:
 - Minimum angular ray separation to resolve two spots from one is:
 $\sin \theta_{\min} = 1.220 \lambda/D$.
 - Since θ_{\min} is small, $\theta_{\min} \approx 1.220 \lambda/D$.
 - D is the diameter of a circular aperture.
 - 1.220 is the first zero of the Bessel function $J_m(x)$.
 - An Airy function results from Fraunhofer diffraction from a circular aperture.
- Straight line pattern:
 - Minimum angular ray separation to resolve two lines from one is:
 $\sin \theta_{\min} = \lambda/D$, or approximately $\theta_{\min} \approx \lambda/D$.

Projection Lithography Requirements

- b = minimum feature size (spot or line)
- $2b$ = minimum period of line-space pattern
- λ = exposure wavelength
- Using $b = f \theta_{\min}$, obtain that $b \approx \lambda/2NA$.
- The depth of focus can be shown to be $d_f = \pm \lambda/2(NA)^2$
- A “voxel” is a volume pixel.
- For highest resolution lithography, desire the tallest aspect ratio voxel.
- Thus, wish to maximize the ratio $d_f/b = 1/NA$.
- SO: it all depends upon the NA of the lens!



Sample Calculation

- Primary reduction camera in WTC-MFL uses a projection lens with $f/6.8$ and $f = 9.5 \text{ in.} = 241.3 \text{ mm}$.
- Lens diameter is $D = 241.3 \text{ mm}/6.8 = 35.5 \text{ mm} = 1.40 \text{ in}$.
- The numerical aperture is $NA = 1/2 * 6.8 = 0.074$.
- For exposure in the middle green, $\lambda = 550 \text{ nm}$.
- Thus, the minimum feature size is $b = 550 \text{ nm}/2 * 0.074 = 3.72 \text{ }\mu\text{m}$ for a line, or $1.220 * 3.72 \text{ }\mu\text{m} = 4.56 \text{ }\mu\text{m}$ for a spot.
- The tightest grating pitch that could be printed using this lens is therefore $2b = 7.44 \text{ }\mu\text{m}$.

Lens Aberrations

- Chromatic aberration
 - Dispersion: change of refractive index with wavelength
- Monochromatic aberrations
 - transverse focal shift
 - longitudinal focal shift
 - spherical aberration
 - coma
 - astigmatism
 - field curvature
 - distortion

Projection Optics

- It is exceedingly difficult to make large NA refractive optics due to aberration limits.
 - The best lenses used in projection lithography have $NA = 0.3 - 0.4$
 - A lens with $NA = 0.50$ is a $f/1.00$ lens: its focal length and effective diameter are the same!
 - The largest NA lenses ever made were a $NA = 0.54$ and a $NA = 0.60$ by Nikon.
- Reflective optics are better suited for large NA applications.
 - But they are physically larger, and usually require close temperature stability to keep their proper contours and alignment.
- Combinations (catadioptric) systems are also used.
 - This is very common in DSW (stepper) lithography equipment.

Contact and Proximity Lithography Resolution

- λ = exposure wavelength
- d = resist thickness
- $2b$ = minimum pitch of line-space pattern
- s = spacing between the mask and the resist

– Contact Printing:

$$2b = 3\sqrt{0.5\lambda d}$$

- At $\lambda = 400$ nm, $d = 1$ μm , obtain $b = 0.7$ μm linewidth.

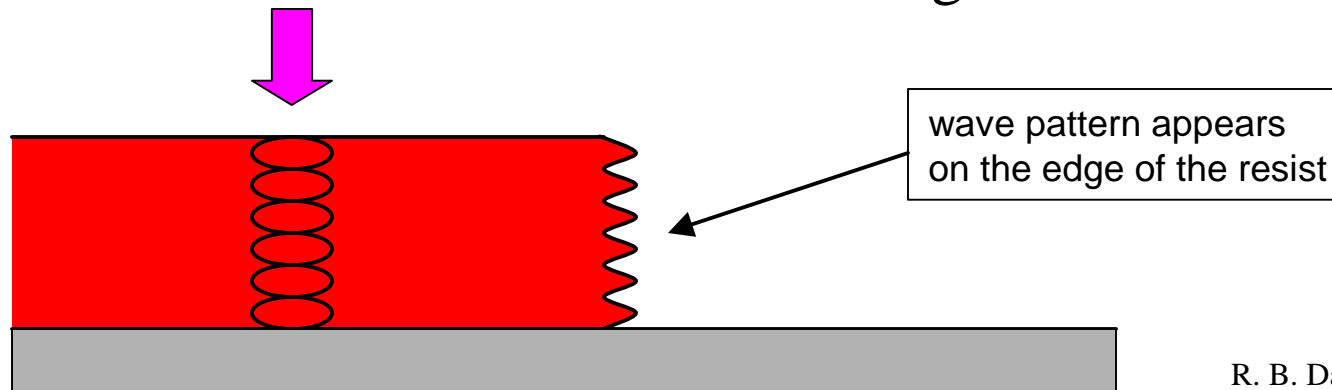
– Proximity Printing:

$$2b = 3\sqrt{\lambda (s + 0.5d)}$$

- At $\lambda = 400$ nm, $s = 10$ μm , $d = 1$ μm , obtain $b = 3.0$ μm linewidth.

Standing Waves - 1

- Short exposure wavelengths can create standing waves in a layer of photoresist. Regions of constructive interference create increased exposure.
- These can impair the structure of the resist, but can be eliminated by:
 - use of multiple wavelength sources
 - postbaking
- Effects are most noticeable at the edge of the resist.



Standing Waves - 2

- Standing waves are enhanced by reflective wafer surfaces.
- If the wafer or substrate is transparent, reflections from the aligner chuck can create standing wave patterns, also.
 - This can be eliminated by using:
 - a flat black chuck (anodized aluminum)
 - an optical absorber under the wafer (lint free black paper)
 - a transparent glass chuck (used on Karl Suss MJB3)
- Exposures can be greatly miscalculated by the presence of standing waves and reflective wafers or chucks.

Photographic Exposure Equation

$$T = \frac{f^2}{SB}$$

T = exposure time in seconds

f = f-number of projection lens

S = ASA or ISO film speed

B = scene brightness in candles/ft²

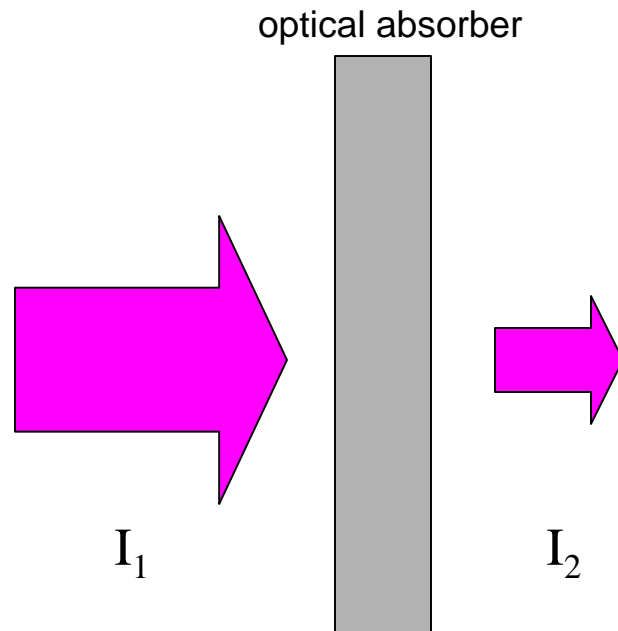
American Standards Association (ASA) film speed is the dose required to produce an optical density of 0.1 in a film media.

German DIN film speed is:

$$\text{DIN} = 10 \log_{10}(\text{ASA}) + 1$$

$$100 \text{ ASA} = 21 \text{ DIN}$$

Optical Absorbance and Density



$$T = \frac{I_2}{I_1}$$

transmittance

$$A = \frac{1}{T} = \frac{I_1}{I_2}$$

absorbance

$$OD = \log_{10}(A)$$

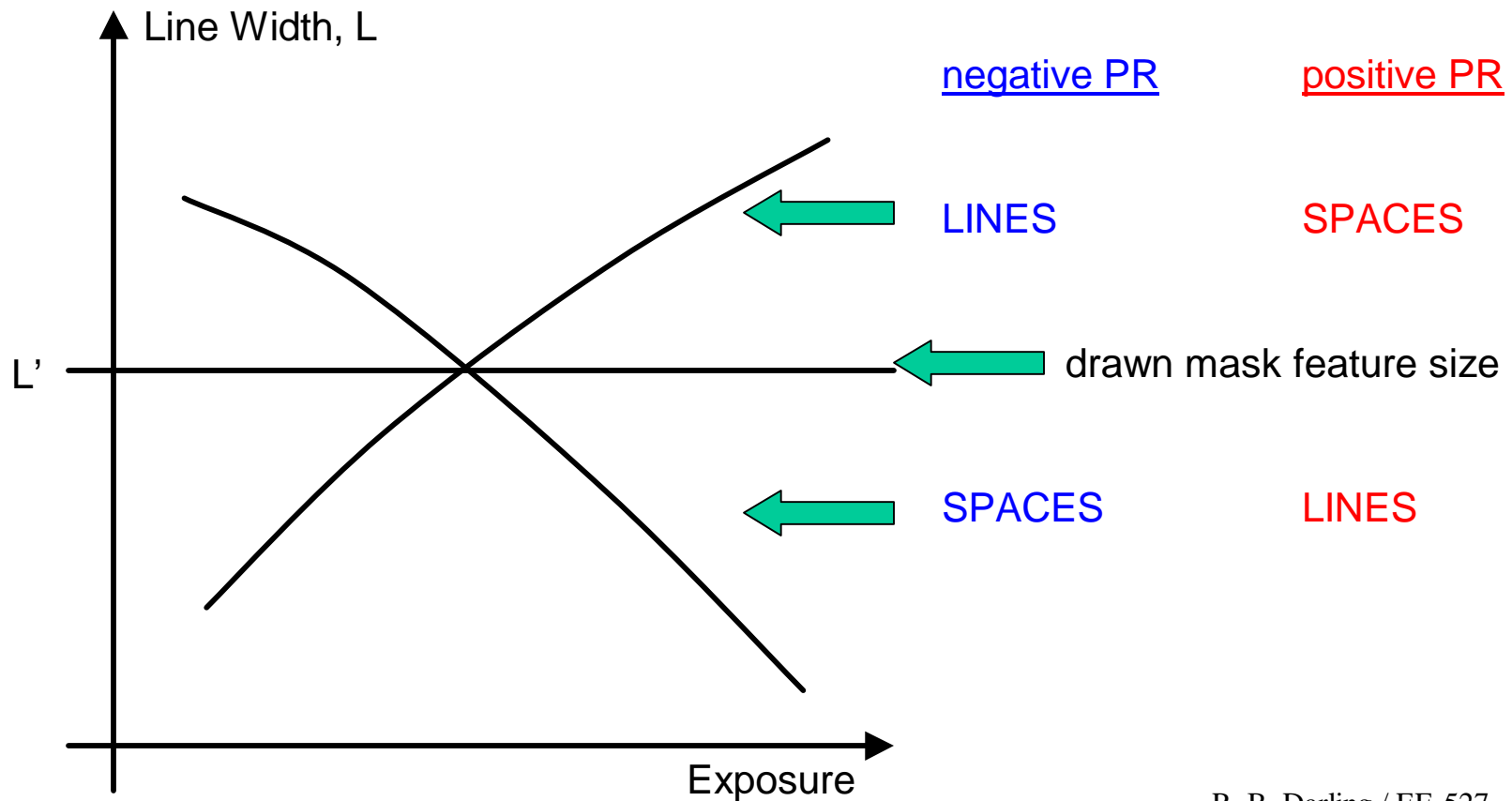
optical density

Typical optical densities:
xerox transparency: $OD = 1$
photographic emulsion plate: $OD = 2-3$
chrome photomask: $OD = 5-6$

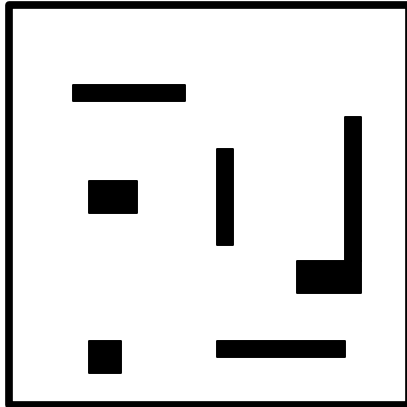
Exposure Latitude

Dimensional Latitude:
(typically want less than 0.05)

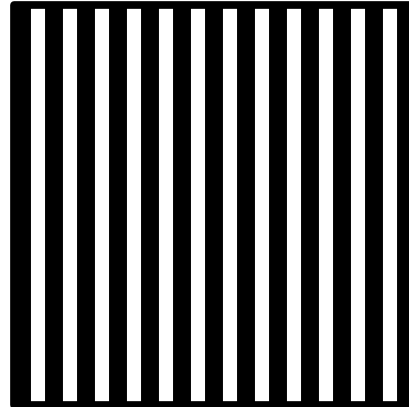
$$d = \left| \frac{L' - L}{L'} \right|$$



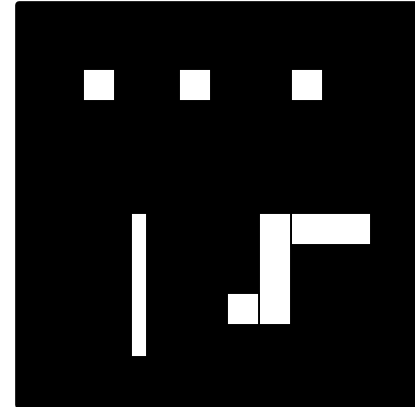
Proximity Exposure Effect - 1



light field



50:50 grating

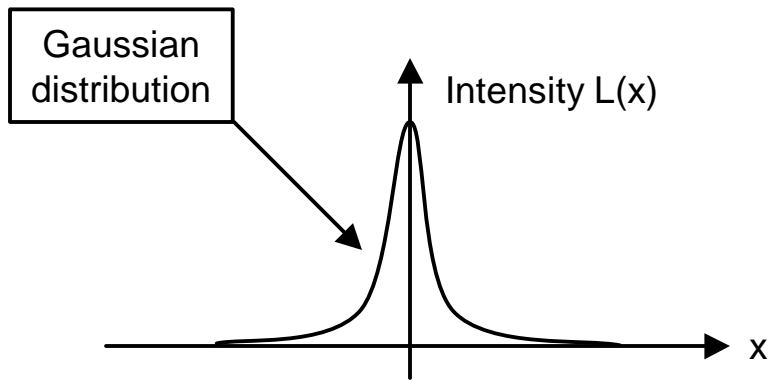
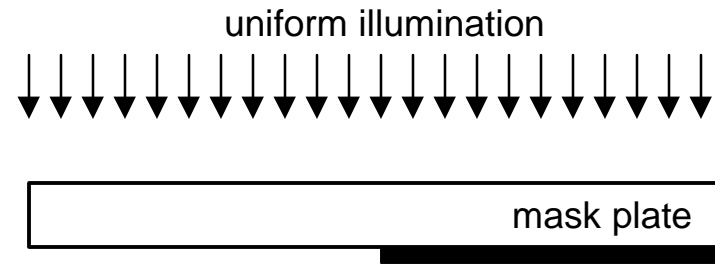
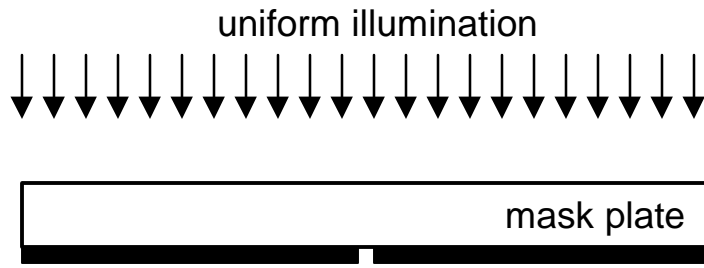


dark field

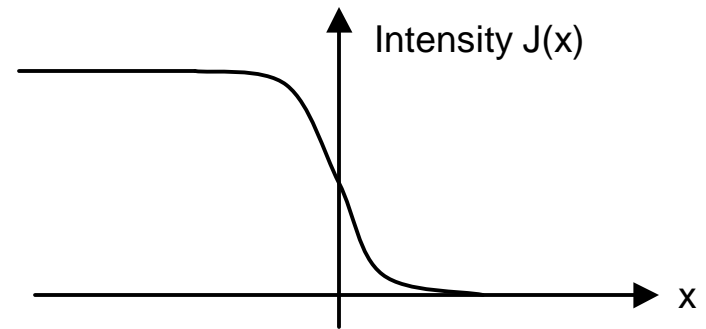
Optimum exposure depends upon the pattern!!!

Adjacent clear (bright) regions add additional exposure to a given region because of overlap from Gaussian tail of the linespread function.

Spread Functions



Line Spread Function $L(x)$



Edge Spread Function $J(x)$

$$L(x) = \frac{dJ(x)}{dx}$$

$$J(x) = \int_{-\infty}^x L(x') dx'$$

Optical Modulation

I = optical intensity, W/cm²

M = optical modulation within a scene or image

MT = modulation transfer factor for an optical element

$$M = \frac{I_{\max} - I_{\min}}{I_{\max} + I_{\min}}$$

$M \rightarrow 1$ when $I_{\min} \rightarrow 0$.

$$MT = \frac{M_{out}}{M_{in}}$$

Modulation Transfer Function

The modulation transfer function (MTF) is the modulus of the Fourier transform of the linespread function:

$$MTF(f) = \left| \int_{-\infty}^{\infty} L(x) e^{-2\pi jfx} dx \right|$$

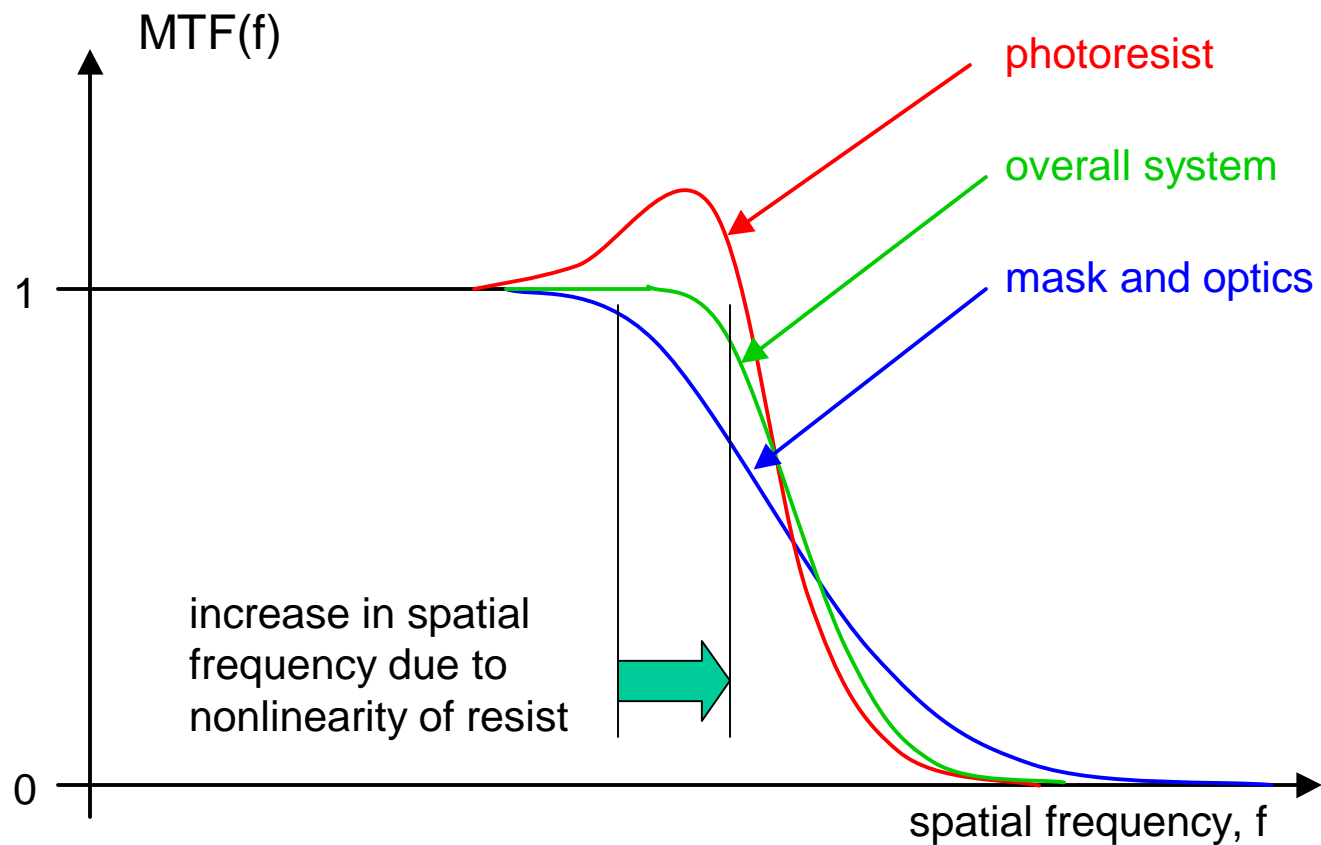
f is the spatial frequency

Optics obeys linear system theory:

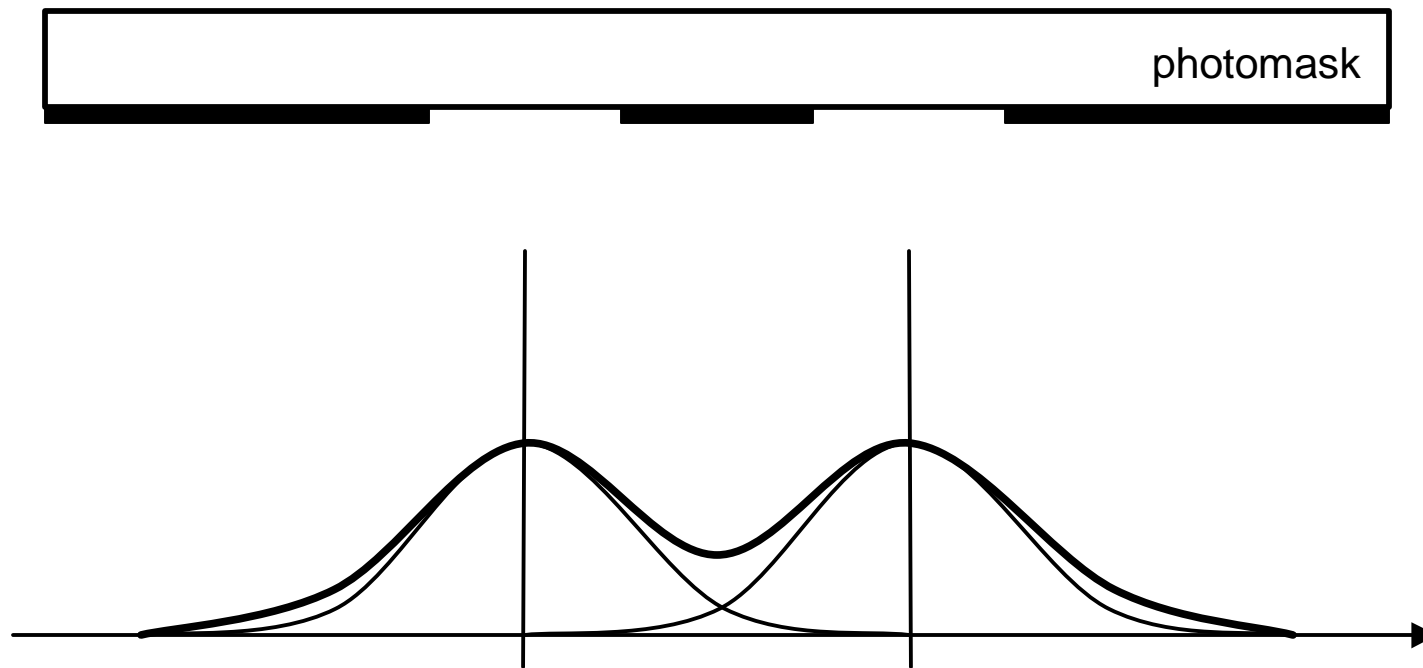
$$MTF(\text{system}) = MTF(\text{element}_1) \times MTF(\text{element}_2) \times MTF(\text{element}_3) \times \dots$$

Modulation Transfer Function in Photolithography

$$\text{MTF}(\text{system}) = \text{MTF}(\text{mask}) \times \text{MTF}(\text{optics}) \times \text{MTF}(\text{resist})$$



Proximity Exposure Effect - 2



Phase Shifting Masks

